



A New Model for Sub-Slab Mitigation for Vapour Intrusion



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*SMART Remediation Conference
23 January 2020 – Toronto, ON*

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Agenda

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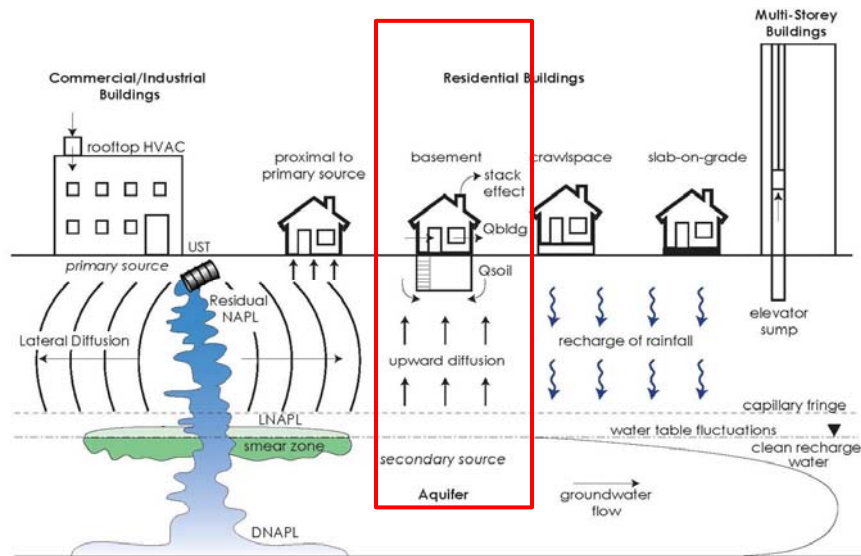
- Case Study
- ESTCP ER201322 Results
- New methods for Mitigation Design



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Vapour Intrusion – Conceptual Model

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Case Study – Sub-Slab Depressurization

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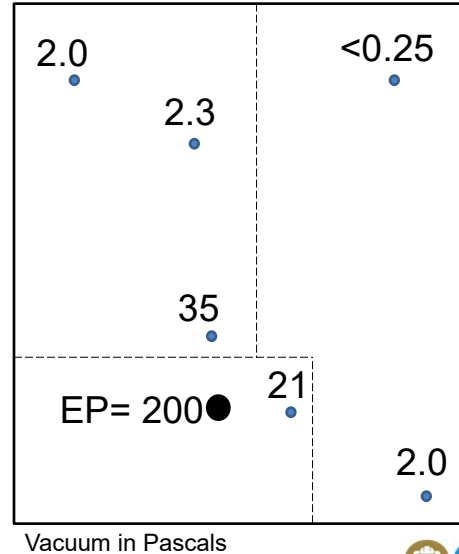


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Am I Safe In My Home?

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- Sub-slab Rn = 13,200 Bq/m³
- Indoor air radon = **450 Bq/m³**
- Attenuation factor = 0.03
- Canada Health Guideline = 200 Bq/m³
- WHO guideline = 100 Bq/m³

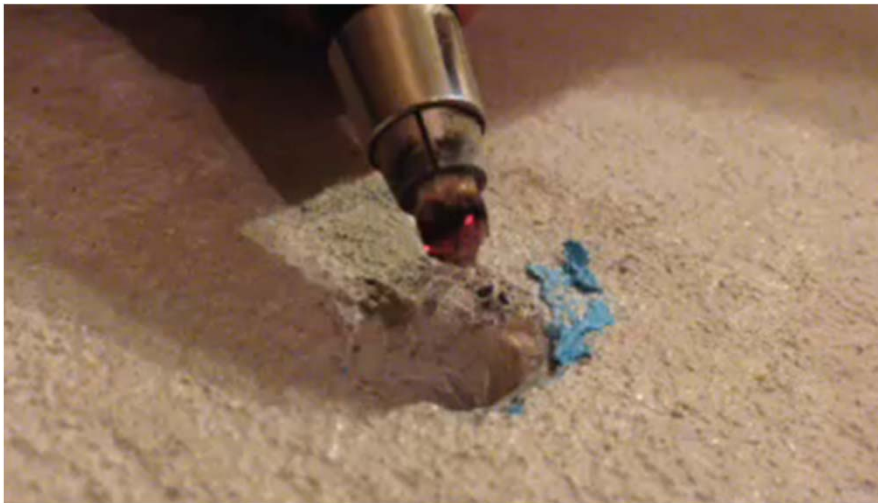


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Flow? Or Vacuum? What matters most?

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30 ft from the suction pit with no measurable vacuum (<0.25 Pa)



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... it depends on the permeability!

$$Q = \frac{-kA}{\mu} \frac{\Delta P}{\Delta L}$$

(Darcy's Law, 1856)

Q = discharge (m³/s)

k = intrinsic permeability (m²)

A = cross sectional area (m²)

P = pressure (Pa)

L = length (m)

μ = viscosity (Pa s)

Unfortunately, it is hard to directly
measure air velocity <70m/day

But flows of 1 m/day are considered
sufficient for SVE (U.S. ACoE, 2002)

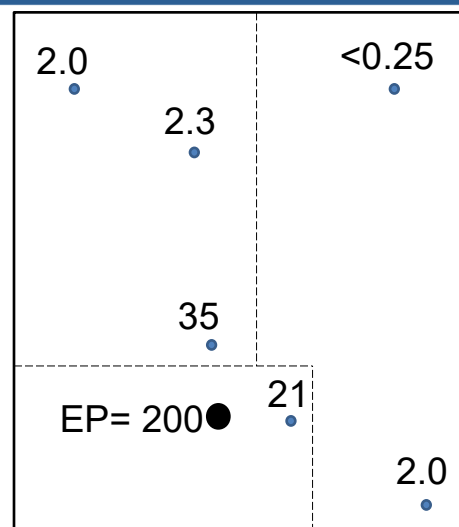
Permeability of silt through gravel spans a range of 1,000,000,000-fold
So, how do we measure permeability?



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Am I safe in my home?

- Canada Health Guideline = 200 Bq/m³
- WHO guideline = 100 Bq/m³
- Indoor air after mitigation = 35 Bq/m³
- Be confident in your design before
collecting indoor air samples



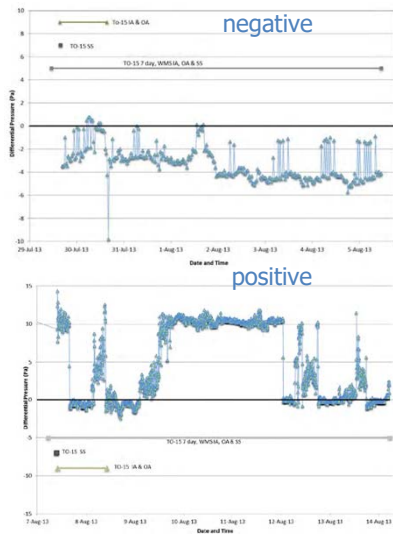
Vacuum in Pascals



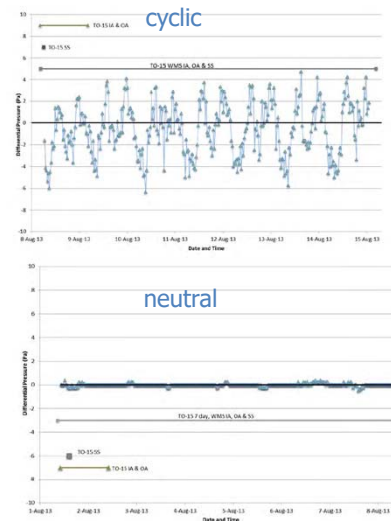
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Cross-Slab Differential Pressure

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What “target vacuum” level is appropriate?

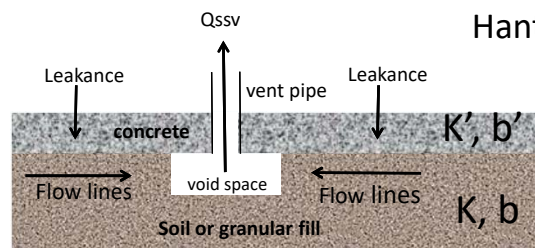


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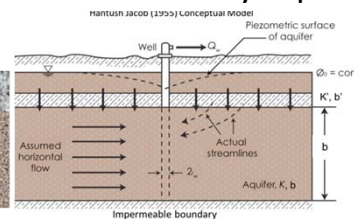
ESTCP ER-2013-22 Mitigation Optimization

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Conceptual Model of Sub-slab Venting



Hantush-Jacob Leaky Aquifer Model



$$T = Kb$$

(T) = Transmissivity below the floor (ft²/day)

(K) = gas conductivity (ft/day)

(b) = thickness (ft)

$$B = \sqrt{\frac{Tb'}{K'}}$$

(B) = Leakance (ft) (this parameter simplifies equations)

Hantush, M.S. and C.E. Jacob, 1955. Non-steady radial flow in an infinite leaky aquifer, Am. Geophys. Union Trans., vol. 36, pp. 95-100.

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Do the Math!

Vacuum versus distance:

$$\text{Vacuum} = \frac{Q_w}{2 \pi T} K_0(r/B)$$

Velocity versus distance:

$$\text{Velocity} = \frac{Q_w}{2 \pi b n B} K_1(r/B)$$

Travel time for sub-slab gas from a given distance:

$$t_{\text{travel}} = \int \frac{\partial r}{v(r)}$$

Proportion of total flow originating below the floor:

$$\frac{Q(r)}{Q_w} = \frac{r}{B} K_1(r/B)$$

Building-specific Attenuation Factor:

$$AF = \frac{Q_{\text{soil}}}{Q_{\text{building}}} = \frac{K' i A}{l w h AER} = \frac{\frac{K b b' \Delta P}{B^2} A}{A h AER} = \frac{T \Delta P}{B^2 h AER}$$

All of these calculations can be done in a spreadsheet



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New Model for Vapour Mitigation

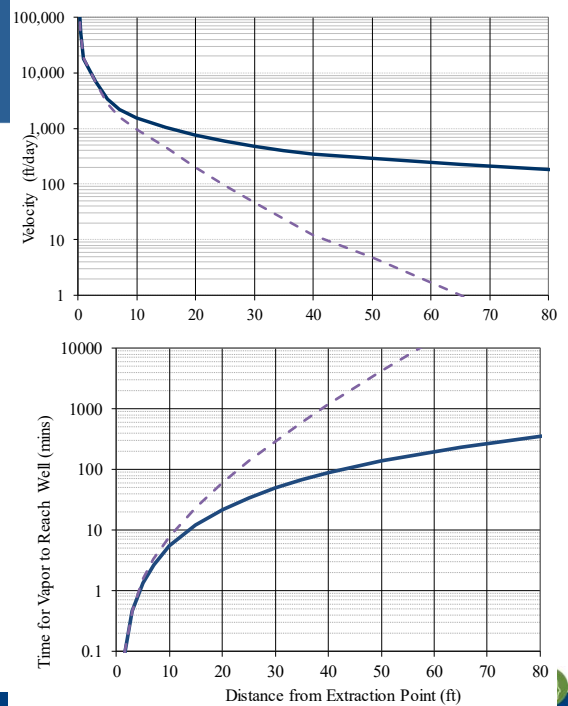
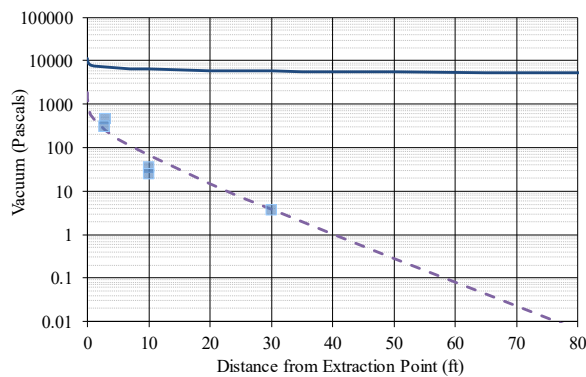
- Vacuum is just one metric > cross-slab ΔP
- Sub-slab velocity > 3ft/day
- Travel time < 2.4 hrs
- Mass removal rate $M_{SSD} > M_{SSFLUX}$
- Do you need to mitigate – developing building specific attenuation factors.



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Pneumatic/Pilot Testing

A simple spreadsheet provides the charts for radial profiles of vacuum, velocity, travel time



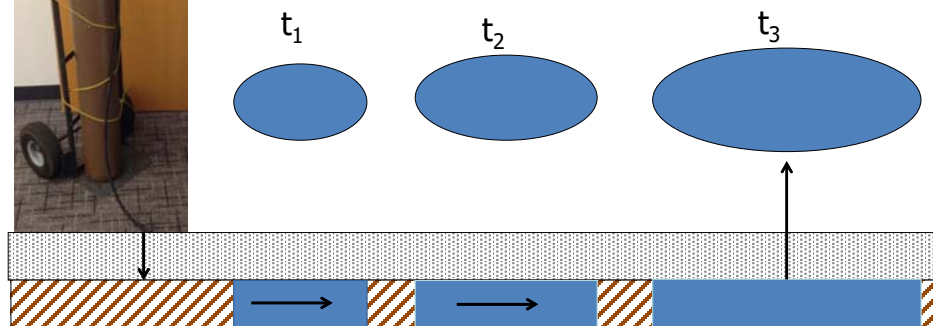
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Inter-Well Helium Tracer Test (velocity vs time)

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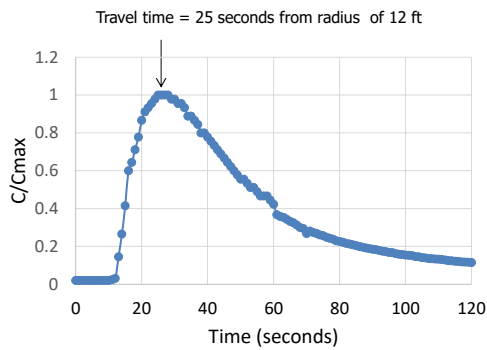


Inject helium into a sub-slab probe near an operating vent-pipe
Monitor Helium in the vent-pipe to get a breakthrough curve

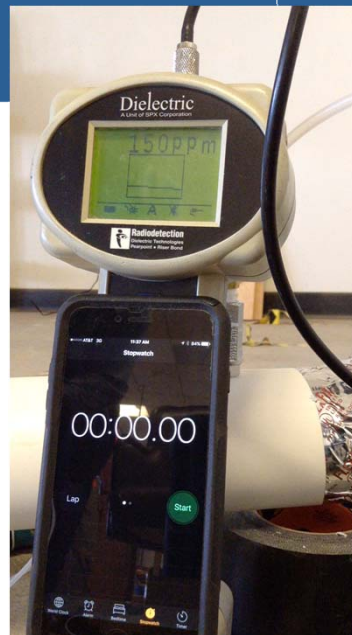


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Helium Inter-Well Test



This data took less than 2 minutes to collect
 These tests are quick, simple and informative
 using low-cost equipment that is easily rented



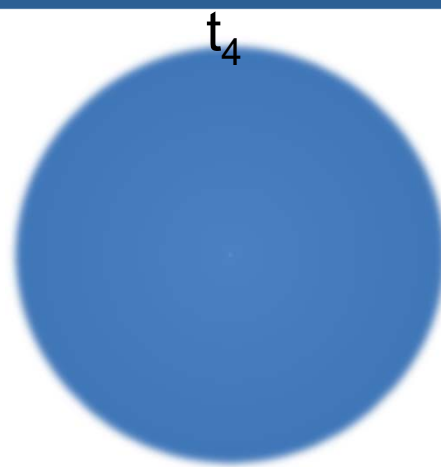
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Helium Flood - (travel time)

Reverse the flow on a vent-fan
 match ΔP and Q to normal operations
 Add helium ($\sim 1\%v/v$ or so)
 monitor transport below the slab

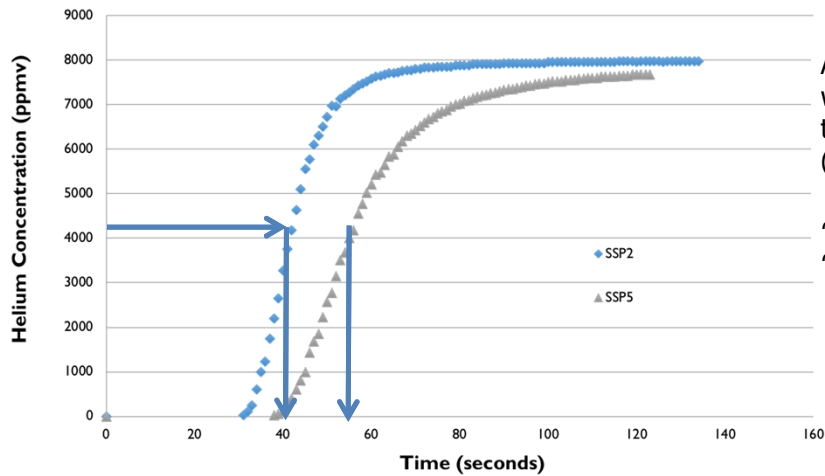


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Helium Flood Results



Average travel time is where He reaches 50% of the injected concentration (4,000 ppmv)

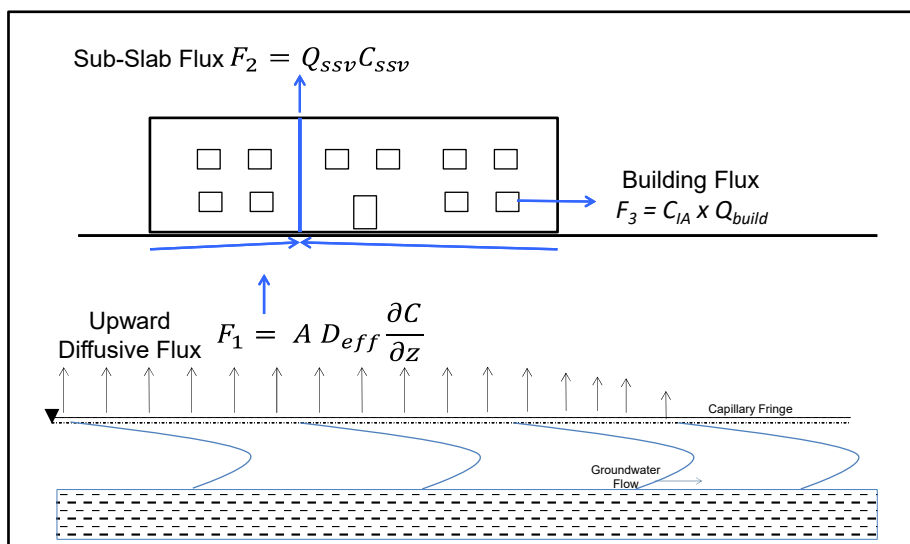
~42 seconds for SSP2
~55 seconds for SSP5

Also very quick, simple and very informative using low-cost equipment that is easily rented



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Mass Flux Monitoring



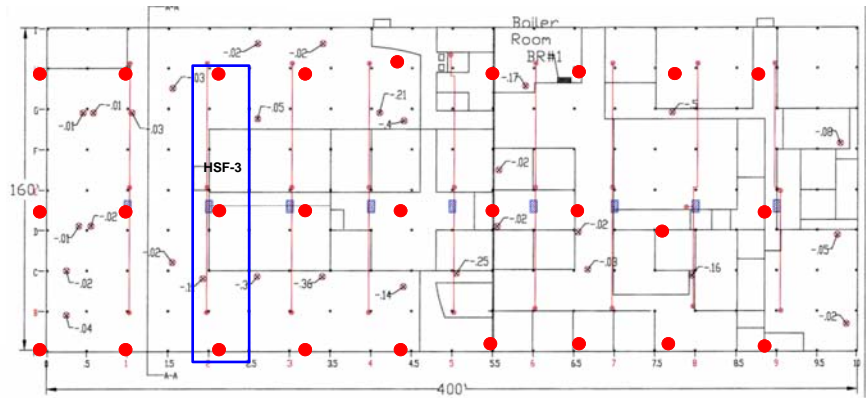
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Mitigation System Optimization

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- Original SSD system design:
- 9 Fans Connected to 3 suction points each – 27 total
- Total system flow
- ~14 m³/min (500 cfm)
- Operating 10 years
- Evaluate Optimization

6,000 m² (64,000SF) Office space

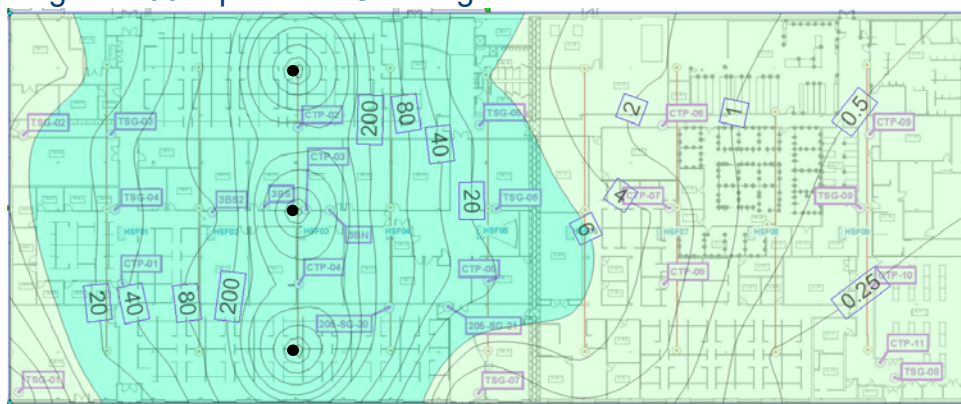


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Mitigation System Optimization

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- Vacuum extends throughout the area of TCE vapours
- Single fan captured 96% of TCE mass flux
- Cost savings of ~90% plus HVAC savings.



Subfloor Vacuum in Pascals



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Attenuation Factor Options

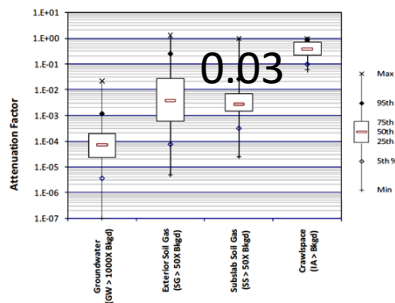
1991 – J&E model

$$\alpha = \frac{\left[\frac{D_T^{eff} A_B}{Q_B L_T} \right] \exp \left(\frac{Q_{soil} L_{crack}}{D_{crack}^{eff} \eta A_B} \right)}{\exp \left(\frac{Q_{soil} L_{crack}}{D_{crack}^{eff} \eta A_B} \right) + \left[\frac{D_T^{eff} A_B}{Q_B L_T} \right] + \left[\frac{D_T^{eff} A_B}{Q_{soil} L_T} \right] \left(\exp \left(\frac{Q_{soil} L_{crack}}{D_{crack}^{eff} \eta A_B} \right) - 1 \right)}$$

2018 - AF from flow and vacuum measurements

$$AF = \frac{T \Delta P}{B^2 h AER}$$

2012 – USEPA Empirical Data



T = transmissivity of the material below the floor (ft²/day)
 ΔP = differential pressure across the floor slab (ft of air column)
 B = leakage of the floor (ft)
 h = height of building (ft)
 AER = air exchange rate (exchanges/day)

McAlary, T., Gallinatti, J., Thrupp, G., Wertz, W., Mali, D. and H. Dawson, 2018. Fluid Flow Model for Predicting the Intrusion Rate of Subsurface Contaminant Vapors into Buildings, Environmental Science & Technology, 2018, 52(15), pp 8438-8445.



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Take-Home Messages

- Vacuum isn't the only factor to show mitigation is occurring.
- Understanding the conceptual site model is key
- There are easy to use tools available
- A Multiple Lines of Evidence (MLE) approach works
- Considerable cost savings can be achieved (4 to 10x reduction)



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